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## Experimental measurements and thermodynamic modeling of CO<sub>2</sub> solubility in the NaCl-Na<sub>2</sub>SO<sub>4</sub>-CaCl<sub>2</sub>-MgCl<sub>2</sub> system up to 150 °C and 200 bar

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#### **Abstract**

To face the climate change, the geological storage of  $CO_2$  in deep saline aquifers has been gaining interest. This study investigates the  $CO_2$  solubility in single-salt solutions containing NaCl, Na<sub>2</sub>SO<sub>4</sub>, CaCl<sub>2</sub> and MgCl<sub>2</sub>. In a first part, an experimental campaign has been performed in an instrumented batch reactor. Acid-base and conductimetric titrations were performed.  $CO_2$  solubility points were obtained for pressure and temperature up to 20 MPa and 423.15 K. The salting-out effect has been studied (at a same ionic force of 3 mol/kg) showing the following order:  $SO_{\%,CaCl_2} < SO_{\%,MgCl_2} < SO_{\%,NaCl} < SO_{\%,Na_2SO_4}$ . In parallel to laboratory experiments, a modelling work has been carried out to calculate the gas solubility. The specific numerical tool named PhreeSCALE was used. The activity coefficient has been calculated using the Pitzer formalism. Interaction parameters for the  $CO_2$ -H<sub>2</sub>O-MgCl<sub>2</sub> and  $CO_2$ -H<sub>2</sub>O-CaCl<sub>2</sub> systems were optimized successfully.

Keywords: CO<sub>2</sub> solubility, single-salt and mixed-salt solutions, thermodynamic modeling, activity coefficient

#### 1. Introduction

CO<sub>2</sub> Capture and Storage in deep geological formation (CCS) is taking part of the panel of possibilities (in addition to the development of renewable energies) to reduce emissions of greenhouse gases to the atmosphere. To develop the CCS field, it is important to predict the quantity of CO<sub>2</sub> that could be stored in the reservoirs [1,2]. Geochemical models are able to predict the solubility of CO<sub>2</sub> in geological formations, which is directly dependent on the brine composition, its temperature and pressure conditions. These models are also supported by the constant acquisition of new experimental data to reinforce databases [3–5]. Many studies have been dedicated to the solubility of CO<sub>2</sub> in pure water. As far as single-salt solution are concerned, the CO<sub>2</sub>-H<sub>2</sub>O-NaCl system is the most investigated with more than 1500 solubility points published for pressures up to 140 MPa, temperatures comprised between 273,15-723,15 K and molalities up to 6 mol/kg. In a much lesser extent, some studies are dedicated to other salts such as CaCl<sub>2</sub>, Na<sub>2</sub>SO<sub>4</sub> and MgCl<sub>2</sub>. To our knowledge, 450 and 400 solubility points are available regarding the CO<sub>2</sub>-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O-H<sub>2</sub>O

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CaCl<sub>2</sub> and CO<sub>2</sub>-H<sub>2</sub>O-Na<sub>2</sub>SO<sub>4</sub> systems, respectively. The CO<sub>2</sub>-H<sub>2</sub>O-MgCl<sub>2</sub> system at high pressure, temperature and salinity has been mostly studied by 3 groups [6–8].

Several thermodynamic models have been proposed to calculate the solubility of  $CO_2$  in pure water and in aqueous brine solutions [9–11]. Among them, the Pitzer model is highly successful to compute the activity coefficients in aqueous solutions rich in dissolved salts. Several authors worked on developing activity coefficient expressions for specific electrolytic systems and for specific operational conditions [11–13]. However, there are still gaps in their ability to cover a wide range of temperatures and chemical compositions of aqueous brines that are encountered in natural deep media targeted for  $CO_2$  geological storage applications. These gaps mainly concerned  $CO_2$  solubility in single-salt systems containing either  $Na_2SO_4$ ,  $CaCl_2$  or  $MgCl_2$  electrolytes near salt saturation, and in salt mixtures.

This study focuses on improving the geochemical modeling of electrolytic systems containing NaCl, CaCl<sub>2</sub>, Na<sub>2</sub>SO<sub>4</sub> and/or MgCl<sub>2</sub>. In a first part, the objective was to generate experimental data on  $CO_2$  solubility in single-salt solutions over a temperature range consistent with the conditions of the targeted storage reservoirs [323,15-423,15 K], for pressures up to 20 MPa and in different salt concentrations [1 to 5 mol/kg]. A discussion of the salting-out effect is also proposed. In a second part, we report the development of a model to calculate the  $CO_2$  solubility in electrolytic single-salt solutions of  $CaCl_2$  and  $MgCl_2$  and in a mixed-salt solution with temperatures up to 473,15 K, pressures up to 40 MPa and salt concentrations near saturation. The Pitzer formalism has been applied due to the high salinity of the solutions. A new set of interaction parameters has been generated to accurately described  $CO_2$  solubility in electrolytic solutions near saturation. All the calculations were performed with the PhreeSCALE geochemical simulation software, which allows calculating the  $CO_2$  solubility using an activity-fugacity approach [14].

#### 2. Material and methods

#### 2.1. Experimental set-up, chemicals and protocol

The names of the compounds, their respective CAS registration numbers, as well as the source and purity of the chemicals used in our work are summarized in Table 1.

Table 1:	list of	chemicals	used in	this	study
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Chemical name	Formula	N° CAS	Source	Purity
Carbon dioxide	$CO_2$	124-38-9	Air Liquide	99.7 %wt
Magnesium chloride	MgCl <sub>2</sub> .6H <sub>2</sub> O	7791-18-6	VWR	100% wt
hexahydrate				
Sodium Chloride	NaCl	7647-14-5	Acros Organics	99%
Sodium hydroxide	NaOH	1310-73-2	Fisher Scientific	46/51 %wt
Calcium chloride	CaCl <sub>2</sub>	10043-52-4	Acros Organics	96%
Hydrochloric acid	HCl	7647-01-0	VWR	$0.1 \pm 2$ % mol/L
Pure water	$H_2O$	7732-18-5	Barnstead	$18.2~\mathrm{M}\Omega.\mathrm{cm}$
			Smart2Pure system	

The acquisition of new CO<sub>2</sub> solubility data is carried out on an experimental laboratory pilot, consisting mainly of a Hastelloy C276 autoclave with a volume of 1 L thermostatically controlled (see Fig.1). It can operate at temperatures between 293,15 and 473,15 K. CO<sub>2</sub> loading in the autoclave is performed using a thermostated volumetric pump (Top Industrie PMHP 200-200), which could operate for a pressure up to 20 MPa and offers automatic pressure compensation after each sampling. Details on the reactor description can be found in a previous publication [15].

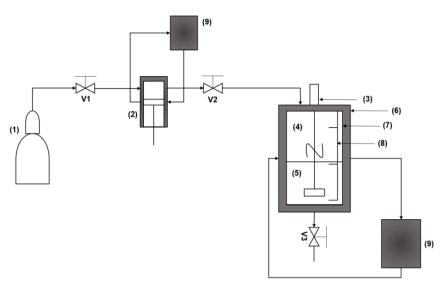


Fig. 1. Scheme of the experimental cell. (1)  $CO_2$  bottle; (2) thermostatic volumetric pump; (3) stirrer; (4) gas phase; (5) aqueous phase; (6) autoclave in Hastelloy C276; (7) double jacket; (8) thermocouples; and (9) thermostatic baths [15].

#### 2.2. *Operating procedure*

Before manipulation, the reactor, the lines and the pump are purged and put under vacuum (see Fig.1). The liquid solution is injected by aspiration, the temperature is set, and the carbon dioxide charged to the desired temperature through the valve V3. Stirring is activated at a speed of 800 RPM. The pressure in the reactor decreases because of the dissolution of  $CO_2$  in the liquid phase. To compensate the pressure drop, the valve V2 is open and then closed again (once the target pressure is reached). Once pressure and temperature equilibrate, agitation is maintained for about one hour (minimum) to ensure the thermodynamic equilibrium of the system. For sampling, a syringe containing a precisely known quantity of sodium hydroxide is connected to the autoclave (valve V3). The valve V3 of the autoclave is open to take aqueous saturated samples. The mass of the sample is obtained by weighing the syringe before and after the end of the sampling. Sodium hydroxide must always be in excess to ensure the total conversion of  $CO_2$  and  $HCO_3^-$  into  $CO_3^{2-}$ , according to reactions (1) and (2), to prevent any outgassing before analysis.

$$CO_{2(g)} + 2 OH^{-}_{(aq)} \leftrightarrow CO_{3}^{2-}_{(aq)} + H_2O_{(l)}$$
 (1)

$$HCO_{3(aq)}^{-} + OH_{(aq)}^{-} \leftrightarrow CO_{3(aq)}^{2-} + H_2O_{(l)}$$
 (2)

The total dissolved inorganic carbon is quantified by titration (see Section 2.3).

For the CO<sub>2</sub>-H<sub>2</sub>O-MgCl<sub>2</sub> system, because the salt dissolved in the aqueous phase will react with the soda as shown in reaction (3), the excess sodium hydroxide must be sufficient to ensure reactions (1), (2) and (3) are complete:

$$MgCl2(aq) + 2 NaOH(aq) \leftrightarrow Mg(OH)2(aq) + 2 NaCl(aq)$$
(3)

As far as the CO<sub>2</sub>-H<sub>2</sub>O-CaCl<sub>2</sub> system is concerned, carbonate ions will directly precipitate with calcium ones to form calcium carbonate:

$$CO_3^{2-} + Ca^{2+} \leftrightarrow CaCO_{3(s)} \tag{4}$$

#### 2.3. Chemical analysis

The measurements of carbon dioxide solubility is made by an automatic titrator using a pH electrode coupled to a conductimetric titration. Contents of the syringe are dosed with 0.1 M hydrochloric acid solution. The measured chemical species present in the syringe are the  $OH^-$  and  $CO_3^{2-}$  ions. From the titration curve, three equivalence points can be detected, as shown in the Figure 2.a. The first equivalence point  $(V_1)$  corresponds to the neutralization of the excess of NaOH in the sample, as shown in reaction (5), although it is not always visible. The second equivalence point  $(V_2)$  corresponds to the conversion of  $CO_3^{2-}$  into  $HCO_3^-$  (reaction 6). Finally, the  $V_3$  equivalence point corresponds to the transformation of  $HCO_3^-$  into  $H_2CO_3$  (reaction 7), which is equivalent to  $CO_{2(aq)} + H_2O$ .

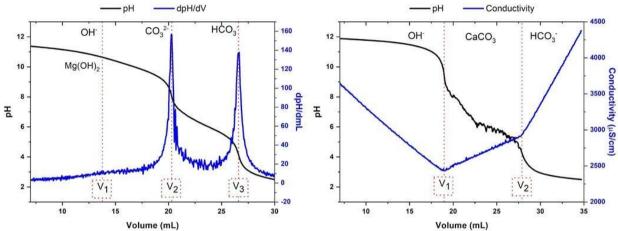


Fig. 2. a) Example of pH and dpH/dV curve vs volume of hydrochloric solution added, b) example of pH and conductivity curves vs volume of hydrochloric solution added.

$$0H^{-}_{(aq)} + H^{+}_{(aq)} \leftrightarrow H_{2}O_{(l)}$$
 (5)

$$CO_{3}^{2-}_{(aq)} + H^{+}_{(aq)} \leftrightarrow HCO_{3}^{-}_{(aq)}$$
 (6)

$$HCO_{3(aq)}^{-} + H^{+}_{(aq)} \leftrightarrow H_{2}CO_{3(aq)}$$
 (7)

Then, the amount of moles of CO<sub>2</sub> can be determined and checked according to the following expression:

$$\eta_{\text{CO}_2} = \eta_{\text{CO}_3^2} - = \eta_{\text{HCO}_3} = \frac{C_{\text{HCI}} (V_3 - V_2)}{1000}$$
(8)

As far as the  $CO_2$ - $H_2O$ - $CaCl_2$  system is concerned, the conductimetric signal is utilized to calculate the  $CO_2$  solubility. The pH signal is recorded to ensure results but is not enough precise. An example of conductimetric result is shown in Fig. 2b. The first part characterized by a decrease of conductivity corresponds to the neutralization of the excess of soda in the sample. The first equivalent point is encountered at the end of this step, where the pH value is around 9. Then, the addition of acid titrant leads to the dissolution of the carbonate precipitate. This is indicated by the second part of the graph, where the conductivity of the solution slightly increases from volume  $V_1$ . The second end-point  $(V_2)$  is reached when the precipitate is totally dissolved following the reaction:

$$CaCO_{3(s)} + 2H^{+}_{(aq)} \leftrightarrow Ca^{2+}_{(aq)} + H_{2}CO_{3(aq)}$$
 (9)

The results reported in this work are the means of five successive titrations performed under each set of equilibrium conditions. To ensure that our sampling process is valid, some criteria have been set, making it easier to identify and exclude possible bad analyzes. These criteria are described elsewhere [3,15].

#### 2.4. Experimental uncertainty

The experimental uncertainty of the present work was evaluated by the analysis of variances (ANOVA) that consists of a statistical method based on repeatability and reproducibility experiments. The principle of the ANOVA methodology was applied and discussed in previous papers [8,15]. The uncertainty was obtained from the analysis of three different experiments (evaluation of reproducibility) performed under the same conditions with five titrations for each experiment (evaluation of repeatability).

#### 3. Experimental results

Fig.3 presents the molality of CO<sub>2</sub> versus pressure (0 to 20 MPa) for pure water and single-salt solutions of NaCl, CaCl<sub>2</sub>, MgCl<sub>2</sub> and Na<sub>2</sub>SO<sub>4</sub> at a temperature of 323,15 K and a salt molality of 1 mol/kg. All curves behaviors are similar: an important solubility increase along with pressure up to 10 MPa and then a plateau. The CO<sub>2</sub> solutility is the highest for pure water. The second highest solubility is obtained for the NaCl solution while the lowest one is obtained for the Na<sub>2</sub>SO<sub>4</sub> one. It illustrates the salting-out effect which corresponds to a decrease of gas solubility when increasing the salinity of a solution. Several studies investigated this phenomenon and highlighted that the salting-out effect depends on the type of electrolyte, its concentration, the temperature and the pressure. However, there is still a lack of understanding.

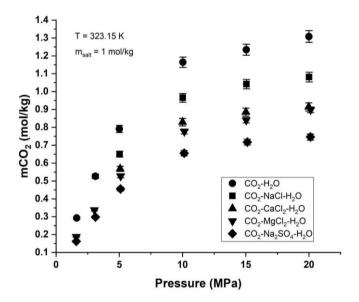


Fig. 3:  $CO_2$  molality versus pressure for pure water and the single-salt aqueous solutions of NaCl,  $CaCl_2$ ,  $MgCl_2$  and  $Na_2SO_4$  at 323,15 K and 1 mol/kg of salt.

Koschel et al., 2006 [16] defined the salting-out effect ( $SO_{\%}$ ) as the calculation of the relative difference between the solubility of gas (here carbon dioxide) in saline solutions (m) and the solubility of the same gas in pure water ( $m^0$ ) under the same conditions of temperature and pressure (Eq.10):

$$SO_{\%} = \frac{100 \times (m^0 - m)}{m^0} \tag{10}$$

Fig.4 presents all the  $CO_2$  solubility data for the NaCl,  $CaCl_2$ ,  $MgCl_2$  and  $Na_2SO_4$  solutions obtained by the LaTEP for ionic strength of 3 mol/kg, temperatures of 323, 373 and 423 K; a range of pressure of 5, 10, 15 and 20 MPa. A total of 48 solubility points are gathered including our previous results [3,8,15,17]. This figure allows us to compare directly the salting-out effect of  $CaCl_2$ ,  $MgCl_2$  and  $Na_2SO_4$  versus NaCl. It is possible to observe the following order:  $SO_{\%,CaCl_2} < SO_{\%,MgCl_2} < SO_{\%,Na_2Cl_2} < SO_{\%,Na_2$ 

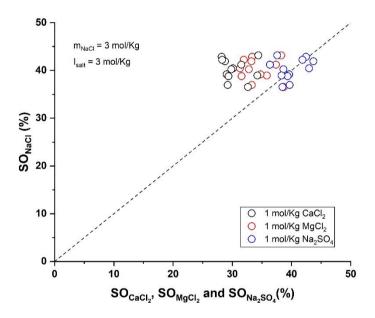


Fig. 4. Comparison of the salting-out effect between the CO<sub>2</sub>-H<sub>2</sub>O-NaCl [17], CO<sub>2</sub>-H<sub>2</sub>O-CaCl<sub>2</sub> [3], CO<sub>2</sub>-H<sub>2</sub>O-Na<sub>2</sub>SO<sub>4</sub> [15] and CO<sub>2</sub>-H<sub>2</sub>O-MgCl<sub>2</sub> [8] at ionic force of 3 mol/kg.

#### 4. Thermodynamic Modeling

#### 4.1. Thermodynamic approach γ-φ

The geochemical calculation code PhreeSCALE allows calculating the  $CO_2$  solubility. It relies on a dissymmetrical approach  $\gamma$ - $\phi$  [18]:

$$m_{CO_2} = \frac{\phi_{CO_2}^{vap} \times P \times y_{CO_2}}{\gamma_{CO_2}^m} \times K_H \times exp\left(\frac{-V_{m,CO_2}(P - P_0)}{RT}\right) \frac{m_0}{P_0}$$
(11)

Where  $m_{CO_2}$  is the molality (mol/kg),  $K_H$  the Henry's law constant (molality scale),  $V_{m,CO_2}$  the molar volume at infinite dilution (cm<sup>3</sup>/mol),  $y_{CO_2}$  the molar fraction (mol/mol) in the gas phase and  $\phi_{CO_2}^{vap}$  which is the fugacity coefficient (unitless) calculated with the Peng-Robinson equation of state. R is the ideal gas constant (8.314 J/mol K),

P is the pressure (bar) and T is the temperature (K). The subscript 0 represents the standard state,  $P_0$  is equal to 1 atm, and  $m_0$  to 1 mol/kg.

 $\gamma_{CO_2}^m$  is the activity coefficient (molality scale) described by the Pitzer formalism [19]. This model explicitly accounts for temperature, species molality and their respective molecular interactions:

$$\ln(\gamma_{CO_2}^m) = 2m_{CO_2}\lambda_{CO_2,CO_2} + \sum_{c=1}^{n_C} 2m_c\lambda_{CO_2,c} + \sum_{a=1}^{n_a} 2m_a\lambda_{CO_2,a} + \sum_{c=1}^{n_C} \sum_{a=1}^{n_a} m_cm_a\zeta_{CO_2,c,a}$$
(12)

 $\lambda$  and  $\zeta$  are binary and ternary interaction parameters, respectively. c and a stand for cations and anions, respectively. Binary and ternary interaction parameters can be described as a function of temperature (Y can be any of the adjustable specific interaction parameter) by the following expression (which is a combination of equations of Christov and Møller, 2004 and Møller, 1988) as proposed by Lach et al., 2016 [14]:

$$Y(T) = A1 + A2.T + A3.T^{2} + A4.T^{3} + \frac{A5}{T} + A6.\ln T + \frac{A7}{(T - 263)} + \frac{A8}{(680 - T)} + \frac{A9}{(T - 227)}$$
(13)

Practically, as few coefficients as possible are used in this equation

#### 4.2. Determination of interaction parameters

First, the interaction parameters for  $CO_2$ - $H_2O$ ,  $CO_2$ - $H_2O$ -NaCl and  $CO_2$ - $H_2O$ - $Na_2SO_4$  systems were optimized and addressed in a previous publication [18]. The model generated through these parameters is capable of reproducing with great precision the experimental data available in the literature [18] over a wide range of  $P - T - m_{salt}$  conditions (namely, 273,15–473,15 K, 0,1–40 MPa and 0–6 mol/kg). Then, taking advantage of these parameters, the interaction parameters for systems containing salt of the  $CaCl_2$  and  $Color MgCl_2$  type were investigated individually. For the  $CO_2$ - $CaCl_2$  system, the solubility data from Messabeb et al., 2017 [3] were used ( $P - T - m_{salt}$  range of 323,15–423,15 K, 5–20 MPa and 1–3–6 mol/kg), totaling 36 experimental points. For the  $CO_2$ - $CaCl_2$  system, the 33 data points published by dos Santos et al., 2021 [8] were used ( $P - T - m_{salt}$  range of 323,15–423,15 K, 1,5–20 MPa and 1–3–5 mol/kg).

The optimizations were performed by coupling PhreeSCALE with PEST [22] according to the principle described in [23]. PhreeSCALE calculates the solubility of CO<sub>2</sub>, using an initial set of values for the specific interaction parameters to be estimated. These calculated results are then compared with the experimental CO<sub>2</sub> solubility values by calculating the objective function that characterizes the deviation with respect to the experimental data. The process is repeated automatically with a new set of interaction parameters until the convergence criteria is satisfied through the method of successive iterations.

#### 4.3. Data analysis calculations

In addition to a graphical evaluation, the average absolute deviations (AAD) between the proposed model  $(m_{CO_2,i}^{cal})$  and the experimental data of  $CO_2$  solubility  $(m_{CO_2,i}^{exp})$  were also calculated according to Eq. 14:

$$AAD_{\%} = \frac{{}_{100}}{{}_{Np}} \sum_{i=1}^{Np} \left( \left| \frac{{}_{CO_{2},i}^{cal} - {}_{CO_{2},i}^{exp}}{{}_{CO_{2},i}^{exp}}}{{}_{CO_{2},i}^{exp}} \right| \right)$$
(14)

The calculated deviations are shown in Tables 3 and 4.

#### 5. Modeling Results and discussions

#### 5.1. Parameterization

For the  $CO_2$ - $H_2O$ - $CaCl_2$  system, the parameterization had to comply with the recent work of Lassin et al. [24] where the partial dissociation of the  $CaCl_2$  electrolyte in the  $CaCl_2$ - $H_2O$  binary system is considered. Consequently, interaction parameters were determined for interactions between  $CO_2$  and the species  $Ca^{2+}$ ,  $CaCl^+$  and  $CaCl_2^{0-}$ . In the  $CO_2$ - $H_2O$ - $MgCl_2$  system, the parameters were obtained for interactions between the  $CO_2$  and  $Mg^{2+}$  species. The parameterization results are reported in Table 2.

	$\mathbf{A_1}$	$\mathbf{A}_2$	$\mathbf{A}_3$	$A_4$	$\mathbf{A}_5$	A <sub>6</sub> A <sub>9</sub>	Reference
$\lambda_{CO_2,Cl}$ -	0	0	0	0	0	0	[18]
$\lambda_{CO_2,Ca^{2^+}}$	1.457807316	-1.45E-03	0	0	-258.1444166	0	This study
$\lambda_{CO_2,CaCl^+}$	-4.055035906	5.84E-03	0	0	708.62675080	0	This study
$\lambda_{CO_2,CaCl_2}{}^{\scriptscriptstyle 0}$	0	0	0	0	0	0	This study
$\lambda_{CO_2,Mg^{2^+}}$	0.5259193460	-1.87E-03	2.60E-06	0	0	0	This study
$\zeta_{CO_2,Ca^{2+},Cl^{-}}$	0	0	0	0	0	0	This study
$\zeta_{CO_2,CaCl^+,Cl^-}$	0	0	0	0	0	0	This study
$\zeta_{CO_2,CaCl_2{}^0,Cl^-}$	0	0	0	0	0	0	This study
$\zeta_{CO_2,Mg^{2+},Cl^-}$	-0.01	0	0	0	0	0	This study

Table 2. Pitzer interaction parameters and coefficients for the temperature dependent polynomial of the Eq. (13) after the optimization.

In the  $CO_2$ - $H_2O$ - $MgCl_2$  system, only the binary interaction parameters were used in a first attempt, in order to minimize the number of parameters. However, without the ternary parameters, the differences between the simulations and experimental data for systems concentrated in salt were large. Thus, the ternary parameter  $\zeta_{CO_2,Mg^2+,Cl^-}$  was added as a constant to improve the capacity of the model, as previously work [18]. As for the  $CO_2$ - $H_2O$ - $CaCl_2$  system, only the temperature dependence was sufficient. Such differences can be attributed to different representations of the binary chemical systems: full dissociation of  $MgCl_2$  versus partial dissociation of  $CaCl_2$ .

#### 5.2. $CO_2$ - $H_2O$ - $Ca^{2+}$ - $Cl^-$ system

Once the new Pitzer interaction parameters were established for the  $CO_2$ - $H_2O$ - $CaCl_2$  system, simulations and graphical comparisons were performed. Figures 5a and 5b show that the isothermal solubilities of  $CO_2$  in the aqueous solutions of  $CaCl_2$  calculated by the model are in agreement with the experimental data at 373 and 423 K. Although the interaction parameters of Pitzer were obtained at pressures between 5 and 20 MPa, the figures show that the model is also able to reproduce correctly the solubility data for pressures below 5 MPa and above 20 MPa.

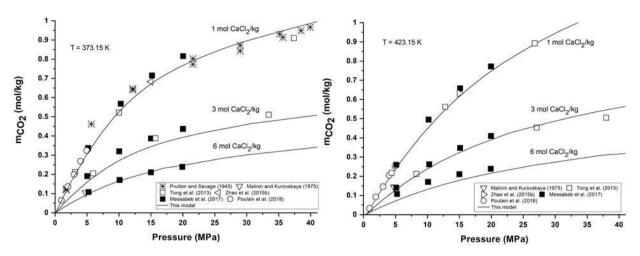


Fig. 5.  $CO_2$  solubilities in aqueous  $CaCl_2$  solution calculated by PhreeSCALE (solid lines) vs. experimental data (symbols) [3,6,7,25–27] a) at 373.15K and b) at 423.15 K.

The model for  $CaCl_2$  was also tested for different temperatures and concentrations. Nearly 370 experimental data from the literature were compared, with an overall mean absolute difference close to 7%. Thus, the proposed model is able to cover a wide range of  $P - T - m_{CaCl_2}$  (293,15-424 K, 0,1-40 MPa and 0-6,3 mol/kg). Overall, the model is capable of reproducing with good quality much of the experimental data present in the literature. However, it is worth noting that several studies have inconsistencies regarding the repeatability of the data [25,28], in addition to error bars or non-existent or greater than 15%, as [29,30].

Table 3. Calculated deviations of CO<sub>2</sub> solubility in aqueous CaCl<sub>2</sub> and MgCl<sub>2</sub> solutions. Np is the number of experimental data.

References	T (K)	P (MPa)	$mCaCl_2$ (mol/kg)	Np	<b>AAD</b> (%)
[25]	348-394	1.5-67.3	1-3.9	115	5.82
[31]	293-323	4.795	0.441-4.495	10	8.25
[31]	373-423	4.795	1.1-6.3	10	11.52
[32]	298-308	0.1	0.22-5.3	16	7.96
[33]	318.15	2.09-15.86	1	8	8.55
[7]	309-424	1.53-37.9	1-5.0	36	8.31
[29]	328.15-375.15	6.89-20.69	1.9-4.8	22	6.49
[6]	323-423	15	0.333-2	18	2.45
[28]	302-338	0.28-11.7	0.1-1	25	8.34
[3]	323.15-423.15	5.0-20	0.1-6.0	36	5.16
[30]	323.15-373.15	5-15.3	0.74-1.94	8	11.81
[34]	323.15-423.15	6.5-59.7	0.7306-2.7526	43	5.60
[27]	323-423	1.2-5.0	1	15	3.61
[4]	323-333	6-40.0	0.2-1	6	2.18
Overall				368	6.86
References	T(K)	P (MPa)	mMgCl <sub>2</sub> (mol/Kg)	Np	AAD (%)
[32]	288.15-308.15	0.1	0.328-3.012	21	2.15
[7]	309.52-424.63	1.25-31.2	1-5.0	39	6.76
[6]	323-423	15	0.333-2	18	1.88
[34]	323.15-423.15	8.23-54.48	0.754-4.29	35	2.62
[8]	323.15-423.15	1.5-20	1-3.0	33	2.21
Overall				146	3.13

#### 5.3. $CO_2$ - $H_2O$ - $Mg^{2+}$ - $Cl^-$ system

Experimental studies of  $CO_2$  solubility data in systems containing magnesium chloride are rare for varied ranges of pressure, temperature and salt concentration. This rarity also extends to thermodynamic modeling works on this system. Three studies, based on the activity coefficient model of Pitzer, propose binary and ternary interaction parameters[6,11,35].

Fig. 6a and 6b show that the simulations carried out with Pitzer interaction parameters determined from experimental data acquired in this work, are also able to represent correctly data from other experimental studies [6,7]. It is at note that Tong et al., 2013 [7] also measured CO<sub>2</sub> solubility at pressures greater than 20 MPa (at 373 K) and that our model remains suitable in these conditions.

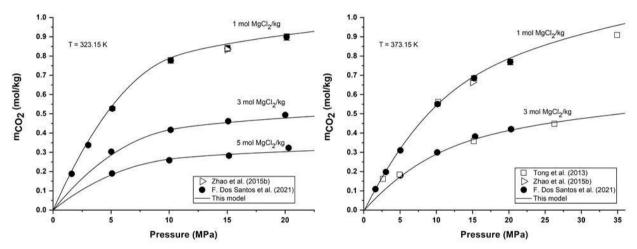


Fig. 6. CO<sub>2</sub> solubilities in aqueous CaCl<sub>2</sub> solution calculated by PhreeSCALE (solid lines) vs. experimental data (symbols) [6-8].

Table 3 presents the results of the mean absolute deviations (AAD) between our model and the different  $CO_2$  solubility data in MgCl<sub>2</sub> aqueous solutions. The calculations were made on one hundred and forty-six experimental data published in the literature. The model as a whole presents an AAD of 3.13% compared to the experimental data. For all the authors studied, except [7], the model had mean absolute discrepancies less than 3%. Data from Tong et al., 2013 [7] at 5 mol/kg show experimental errors that can vary between 1 and 10%; the presented AAD of 6.76% resides in the experimental errors presented by the author. Thus, the model is capable of covering a wide range of  $P - T - m_{MgCl_2}$ , 288-424 K, 0,1-54,5 MPa and 0-5 mol/kg.

Our model was also compared to the 35 experimental points by Mousavi Belfeh Teymouri, 2017 [34] who obtained solubility data for pressures greater than 20 MPa (up to 54 MPa). Most of the data points are therefore outside of the pressure range considered for model optimization and yet, the AAD obtained is less than 2.7%. This shows the robustness of our model and its extensibility to pressures greater than 20 MPa.

#### 5.4. $CO_2$ - $Na^+$ - $Ca^{2+}$ - $Cl^-$ - $H_2O$ system

As a continuation of our work to model CO<sub>2</sub> solubility in pure water and single salt systems (CO<sub>2</sub>-H<sub>2</sub>O-NaCl, CO<sub>2</sub>-H<sub>2</sub>O-Na<sub>2</sub>SO<sub>4</sub>, CO<sub>2</sub>-H<sub>2</sub>O-CaCl<sub>2</sub> and CO<sub>2</sub>-H<sub>2</sub>O-MgCl<sub>2</sub>), we focused on complex chemical systems containing salt

mixtures. In the case of the  $CO_2$ - $H_2O$ -NaCl-Na<sub>2</sub> $SO_4$  system,  $CO_2$  solubility data were measured and compared  $t^2o$  the model, leading to AAD values of less than 4% [18].

References	T (K)	P (MPa)	mNaCl (mol/kg)	mCaCl <sub>2</sub> (mol/kg)	Np	AAD (%)
[33]	318.15	2.46-16.02	0.951	0.505	8	11.06
[6]	323 - 423	15	1.06 - 2.9856	0.217-0.666	24	2.85
[5]	323 - 423	1.2-5.0	1.2	0.2	24	2.47
[4]	333 - 453	6-40.0	1.2	0.2	10	2.29
Overall					66	4.67

Ultimately, the model was also tested on the CO<sub>2</sub>-H<sub>2</sub>O-NaCl-CaCl<sub>2</sub> system, using data collected in the literature. Table 4 shows that the model satisfactorily reproduces the data presented by [4,5,36]. More specifically, Figures 7a and 7b illustrate the comparison between the model and the data from [5] and [4], respectively.

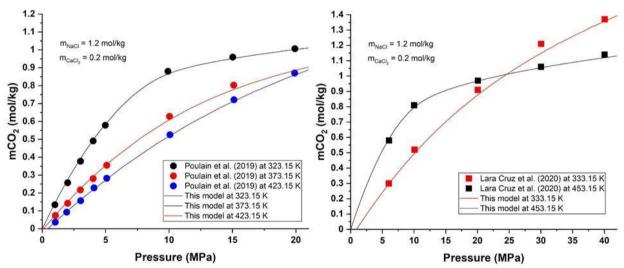


Fig. 7. CO<sub>2</sub> solubilities in aqueous NaCl-CaCl<sub>2</sub> solution calculated by PhreeSCALE (solid lines) vs. experimental data (symbols) [4,5].

#### 6. Conclusions

This study gathers experimental data of  $CO_2$  solubility in NaCl, Na<sub>2</sub>SO<sub>4</sub>, CaCl<sub>2</sub> and MgCl<sub>2</sub> aqueous solutions. Various concentrations were considered, up to salt solubilities; the temperature ranged from 303 K to 423 K and the pressure ranged from 1.5 to 20 MPa. The salting-out effect has been studied (at a same ionic force of 3 mol/kg) showing the following order:  $SO_{\%,CaCl_2} < SO_{\%,MgCl_2} < SO_{\%,NaCl} < SO_{\%,Na_2SO_4}$ . In parallel to laboratory experiments and a bibliographic data collection, a modeling work has been carried out to calculate the gas solubility. The specific numerical tool named PhreeSCALE was used to calculate activity coefficients according to the Pitzer formalism. Interaction parameters for the  $CO_2$ -H<sub>2</sub>O-MgCl<sub>2</sub> and  $CO_2$ -H<sub>2</sub>O-CaCl<sub>2</sub> systems were optimized.  $CO_2$  solubility in these two systems, as well as in the mixed-salt system (1,2 mol/kg NaCl and 0,2 mol/kg CaCl<sub>2</sub>) could be modelled successfully. Comparison to the literature results in overall AAD smaller than 10% and shows the extrapolation capabilities of the model.

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