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# Semi-analytical model of brine and CO<sub>2</sub> leakage through an abandoned plugged well. Applications for determining an Area of Review and CO<sub>2</sub> leakage rate.

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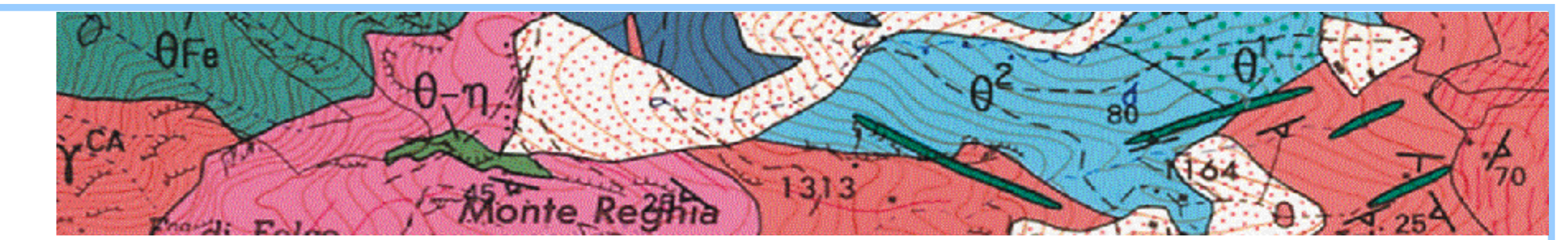
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# Semi-analytical model of brine and CO<sub>2</sub> leakage through an abandoned plugged well. Applications for determining an Area of Review and CO<sub>2</sub> leakage rate



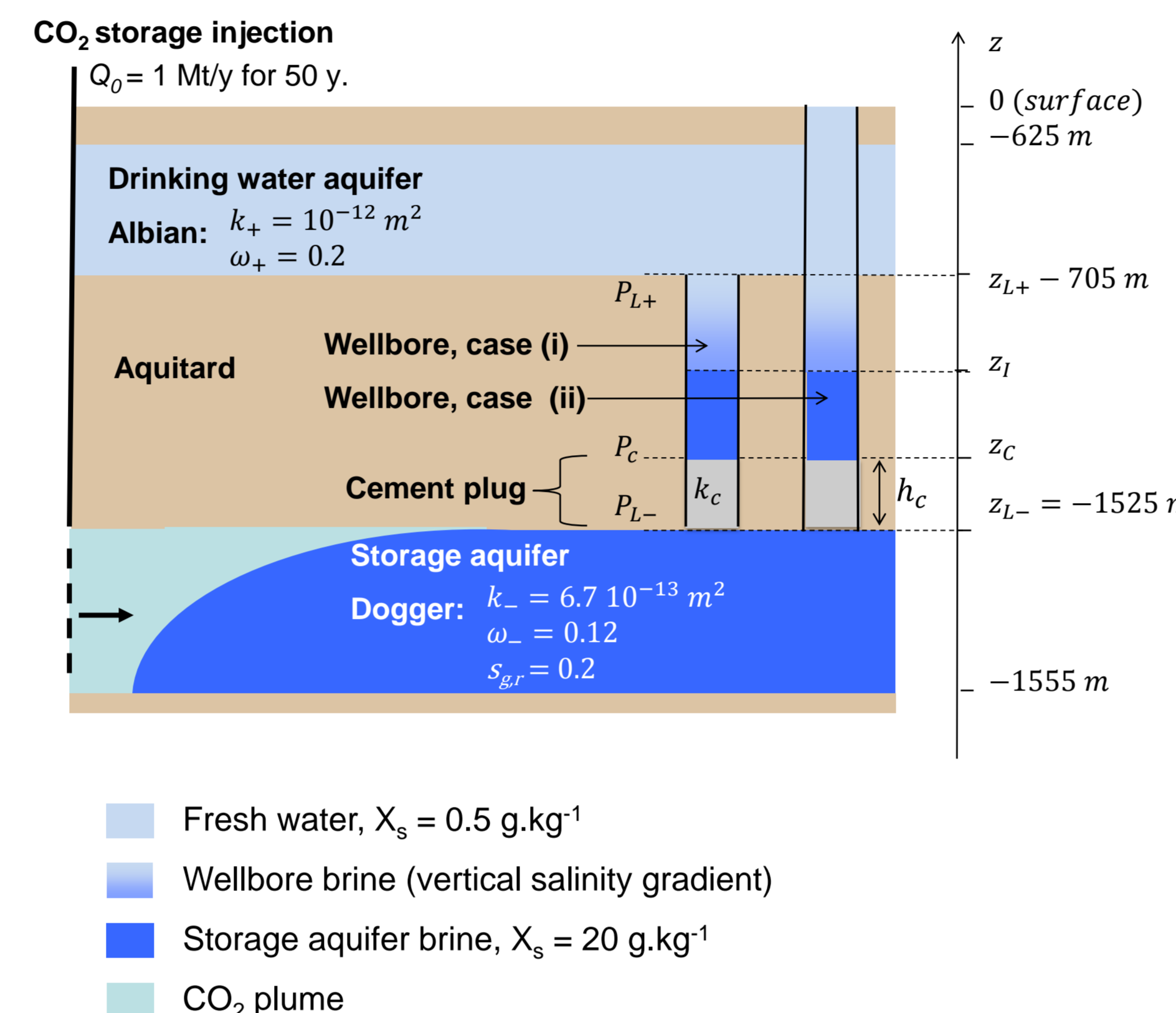
## Introduction

- > Many CO<sub>2</sub> storage projects target **deep saline aquifers** located in sedimentary basins. In these regions, historical oil & gas operations have often left abandoned wells with sometimes undetermined plugging records
- > The risk of **leakage through abandoned wells** should therefore be assessed, notably for preventing two adverse effects: (i) **the pollution of overlying fresh water aquifers** through the migration of saline brine, and (ii) **the emission of large fluxes of CO<sub>2</sub> in the atmosphere**. The present model may be used for describing both

## Position of the model

- > Existing **semi-analytical models** can estimate the leakage flow rate of brine, possibly followed by CO<sub>2</sub>, from the storage aquifer to overlying ones (cf. publications by Nordbotten, Celia and co-authors, 2004-2009)
- > Based on these approaches, this work includes several novelties:
  - It considers the **pressure increase** under the leak when the **dense saline brine** from the storage reservoir progressively fills in the leak and replaces the native fluid of the wellbore, and then its decrease when the **lighter CO<sub>2,g</sub>** breaks through
  - The leak is composed of an **open wellbore** and a **porous column of varying height & permeability**, which may represent various leaks, from an empty wellbore to a flow in a porous media such as the annular cementation. It either reaches the surface or an overlying aquifer

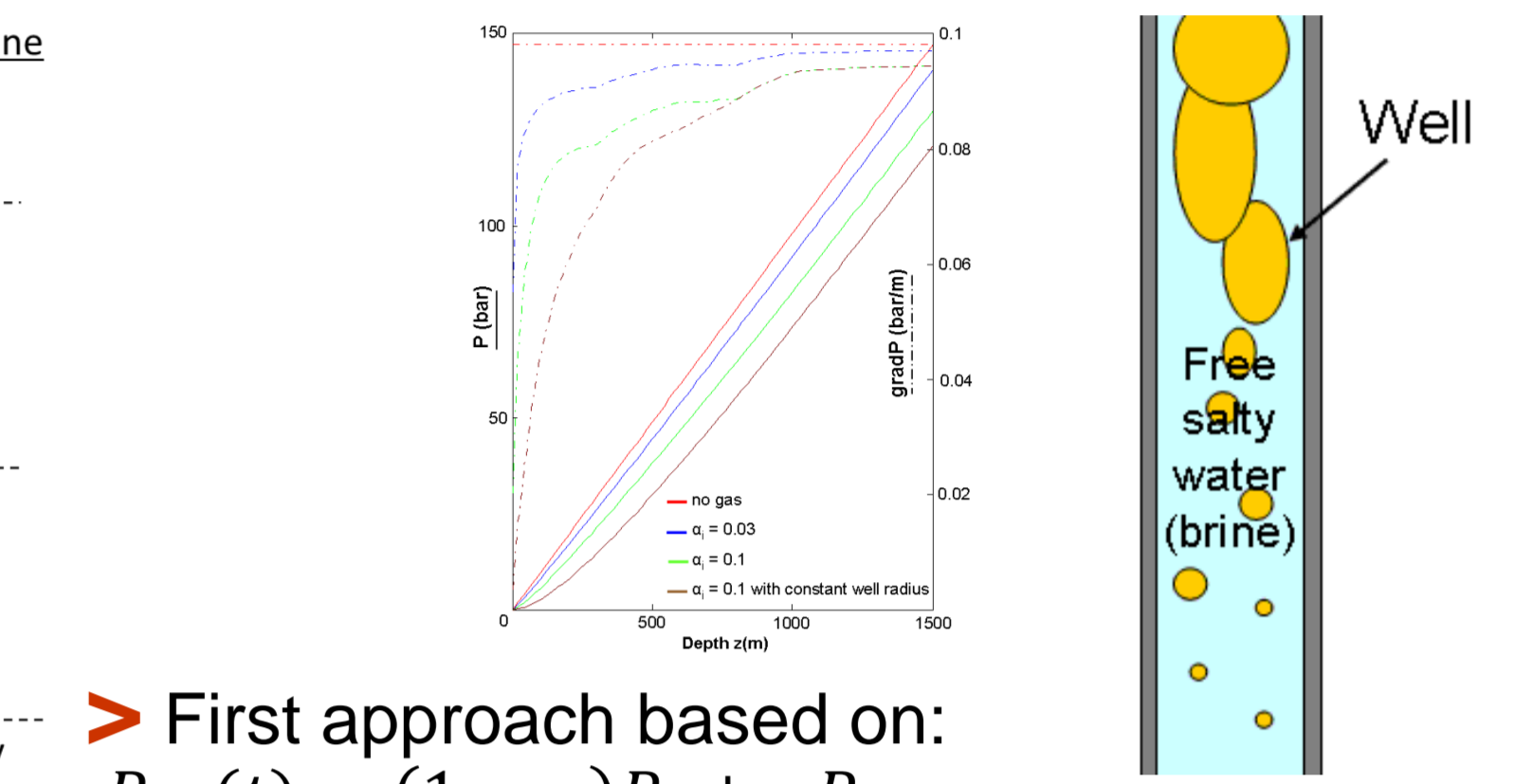
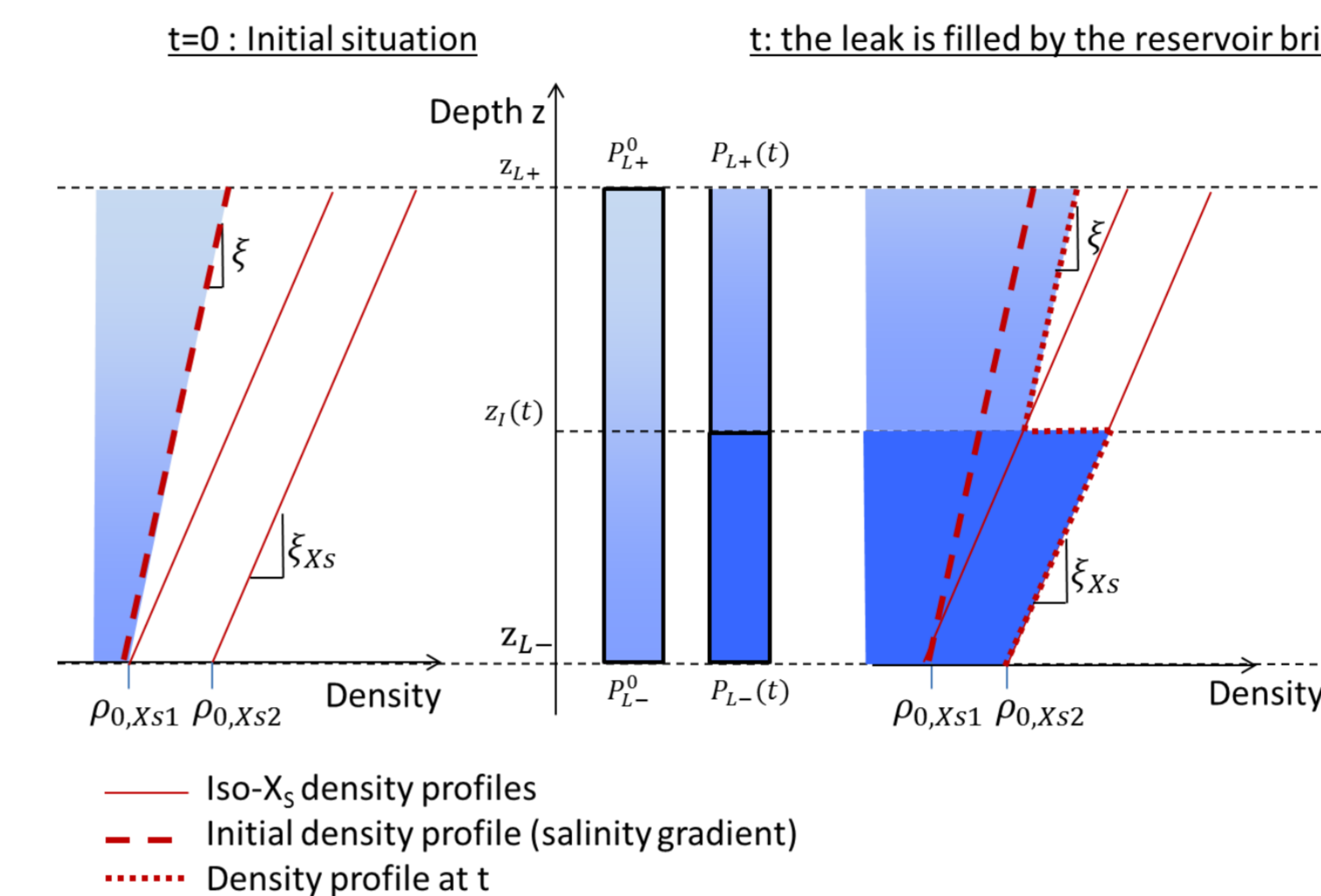
## Schematic layout & Paris basin case main data



## Pressure under the leak modeling

> During the brine leakage

> During the CO<sub>2</sub> leakage

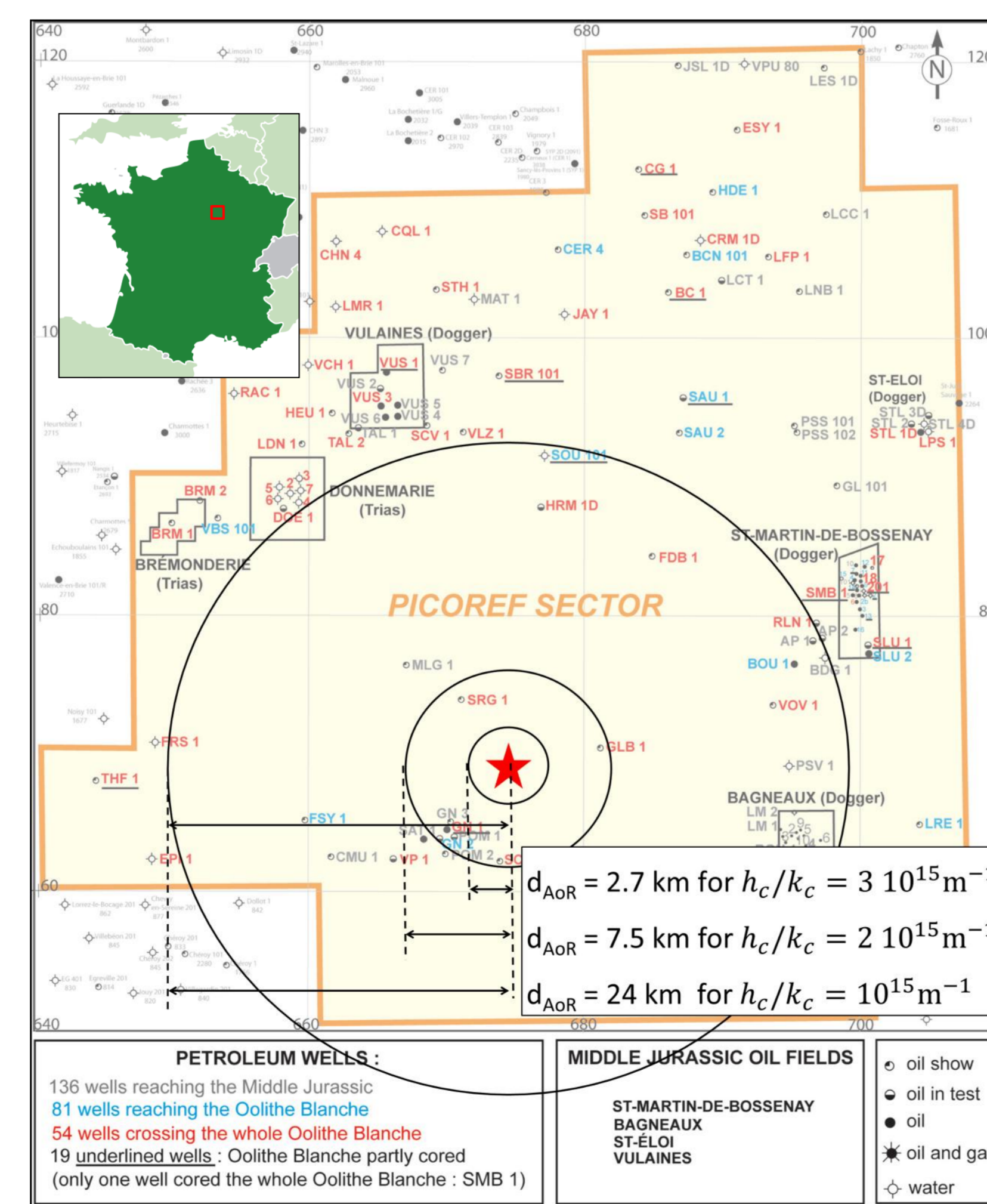
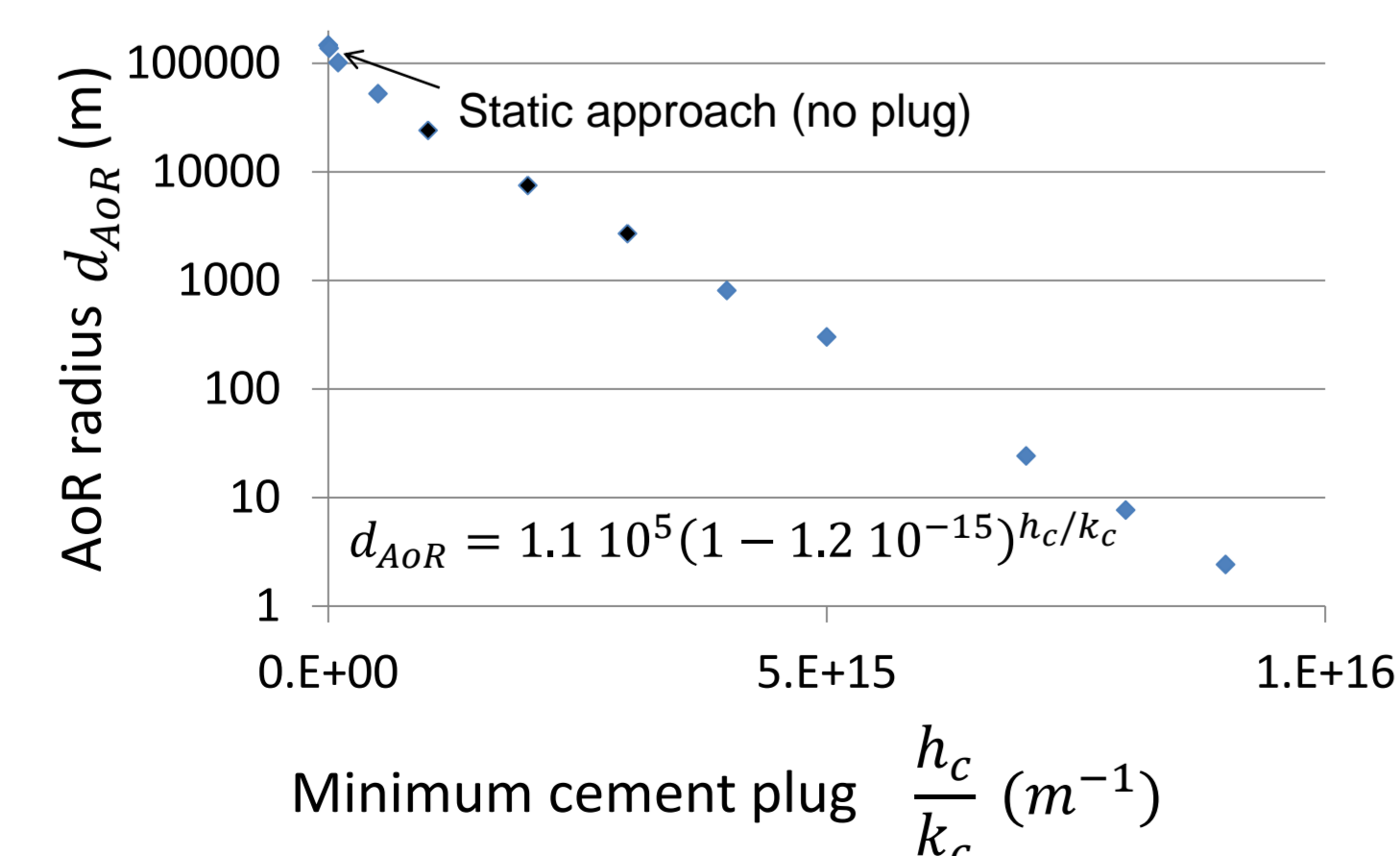


- > During the brine leakage, a pressure increase under the leak  $P_L(t)$  is considered due to the **density difference** between native and reservoir brine salinities.
- > Paris basin case: when the Dogger brine reaches the Albian aquifer,  $P_L$  has increased of 0.04 MPa

- > First approach based on:  $P_L(t) = (1 - \alpha)P_1 + \alpha P_2$
- where:
  - $P_1, P_2$  are the pressure for the column entirely filled with brine resp. CO<sub>2</sub>
  - $\alpha \in [0,1]$  is a coefficient proportional to the leakage rate  $Q_{L,CO_2}$  and inversely proportional to the CO<sub>2</sub> uprising speed in the wellbore (assumed to be 0.16 m.s<sup>-1</sup> in average). Cf. Wertz, F., Audigane, P., Bouc, O., 2009, CO<sub>2</sub> -Thermodynamic Model in a Leaking Well, En. Procedia 1 (2009) 1791-1798

## Application (i): Determining an Area of Review

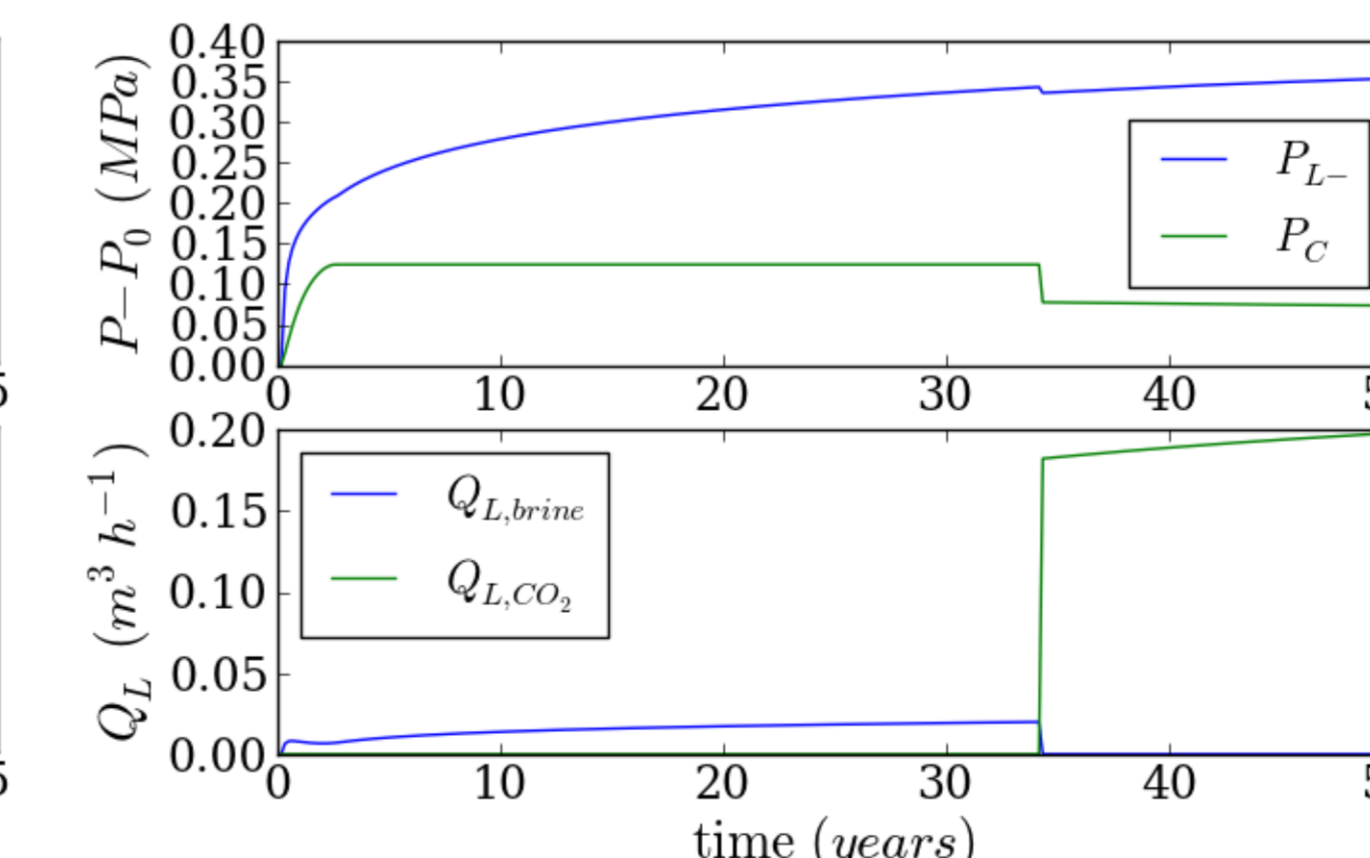
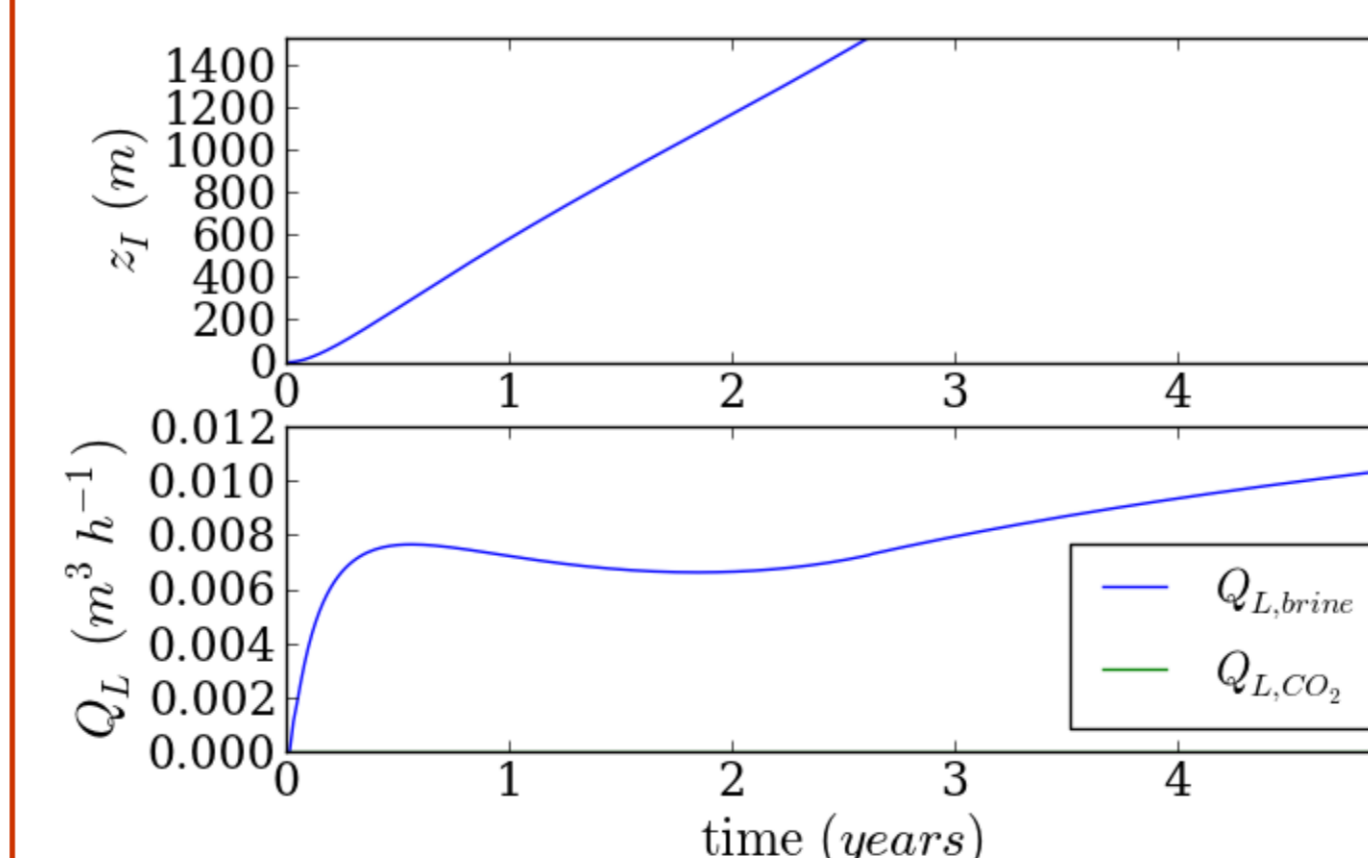
- > "Area of review" defined as the area where the pressure changes due to the injection can drive the reservoir brine up to a shallower aquifer of interest
- > Application of the injection scenario to the PICOREF sector in the Paris basin (France). The Oolithe Blanche layer, or "Dogger", is used for CO<sub>2</sub> storage. 135 abandoned wells reach this layer and the overlying Albian aquifer in the sector.
- > Prioritization of the areas to review supposing a minimum cement plug height on permeability ratio



Adapted from Delmas, J., Brosse, E., Houel, P., 2010. Oil & Gas Sci. and Tech. Vol. 65 (2010), No. 3, pp. 405-434

## Application (ii): CO<sub>2</sub> leakage to the surface

- > Same case study as Application (i), except that the leak directly connects the Dogger aquifer to the surface. A weak cement plug ( $h_c = 1m; k_c = 10^{-13}m^2$ ) is considered in the leak, which is located 5 km away from the injection point
- > Borehole filling until 2.6 years
- > CO<sub>2,g</sub> breakthrough at 34 years



- > Dense Dogger brine progressively fills the leak up to the surface; the pressure under the leak increases
- > Visible cusp on the brine leakage rate due to the end of the pressure increase
- > Visible decrease of the pressure under the column of fluid after its filling with a lighter mixture of brine and CO<sub>2,g</sub>
- > Due to the low CO<sub>2</sub> viscosity, the CO<sub>2</sub> leakage rate largely increases compared to the previous brine leakage rate

## Conclusions

- > The model describes the leakage of brine through the leak, and of CO<sub>2,g</sub> as a first approach. Compared to the state of the art, it adds the possibility of accounting for **density change** within the leak, due to either the incoming of **dense brine** or **light CO<sub>2</sub>**
- > It shares the advantages (immediate computation) and drawbacks (homogeneous layers) of **semi-analytical models**
- > Compared to a static approach, this dynamic model enables less conservative estimation of the "Area of Review", by including effects of **cement plugs**, of **brine density differences** and of leakage-induced pressure effects